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Improved Back EMF of Rotor Position Detection of a Sensorless BLDC Motor

Kaushik Kumar Pandey P.G. Student [Power Electronics], Department of EX, NIIST, Bhopal, M.P., India Jitendra Singh Bhadoriya Assistant Professor, Department of EX, NIIST, Bhopal, M.P., India

Abstract:

This paper represents an improved direct back emf detection method which is used further in the rotor position detection of a sensorless brushless dc (BLDC) motor. It is desirable in any kind of machine to use a method which is less dependable on the sensors and complex circuits, so in this paper a sensorless method is used to commutate and trigger the inverter connected to BLDC motor. Hall effect signals gives the information of the operations in the BLDC motor in this paper hall effect signals are used for the gate pulses for the inverter. Rotor position determination plays an important role in the improvement of the satisfactory operation of the motor so it is desirable to get the proper information of the rotor position or rotor angle. In this paper rotor position is determined by the Zero Crossing Detection (ZCD) of back emf. Unlike old methods of calculating Back emf of the BLDC by creating a virtual neutral point, a complimentary method is used. This method provides a wide range of speed. A pre conditioning circuit is proposed to rectify the back emf at very low speed. The rotor position can be determined even in stand still condition.

1. Introduction

A permanent magnet synchronous motor (PMSM) has been widely used in industrial automation and consumer electric appliances due to high power density, high reliability, maintenance free nature, and silent operation. A PMSM is classified into two types based on the back electro-motive force (BEMF) waveform shape. One variety with sinusoidal BEMF is known as a brushless AC (BLAC) motor and the

other with trapezoidal BEMF is a brushless DC (BLDC) motor .

A BLAC motor which is typically excited by a sinusoidal current requires continuous rotor position, thus a position sensor with high resolution such as an encoder or a resolver is used. On the other hand, a BLDC motor which is powered by a rectangular current requires only six discrete rotor position, thus low-cost hall sensors are usually used.

The structure of a BLDC motor is shown in Fig. 1. BLDC drive system consists of a BLDC motor, control circuit and sensor for position information.



Figure 1: Schematic diagram of a BLDC Motor

In a BLDC motor drive system position information is obtained from the Hall Effect sensor output.

Previously Rotor position information is determined by indirectly sensing the back emf from one of the three motor terminal voltages of three phase motor. The two typical control methods for BLDCM is square wave control method

and the other is sinusoidal current control method. The accuracy for the position information is different between two control methods. In this paper proposed technique is the "Back EMF ZCD" is used to determine the Rotor Position Detection Technique

for Sensor less BLDC Motor control. Back EMF is obtained from the supply, with the voltage divider connected with low pass filters and comparator circuit. When this Back EMF is send to zero crossing detector circuit a positional pulse used for rotor position detection is obtained. The Positional Pulse is compared with the hall pulse and their phase difference is obtained. When the motor is in standstill conditions the back EMF will be zero, so rotor position cannot be determined. To determine the rotor position at both in standstill and running conditions back EMF ZCD method is used.

2. Proposed Direct Back EMF Sensing

The phase back EMF voltage is referred to neutral point of the motor. Since the center point of the motor is typically not available, the commonly used method reconstructs the neutral voltage information. Figure 2 shows the detection circuit based on motor virtual neutral voltage. Voltage dividers and low pass filters are necessary to process the signals. The low pass filter will introduce a phase delay for the zero crossing of the phase back EMF. The first problem with this scheme is low signal/noise ratio at low speed, since the back EMF amplitude is directly proportional to the motor speed. The second problem is that the low pass filter at high speed introduces too much phase delay. Consequently, the conventional back EMF sensing method is only good for narrow speed range.

For BLDC drive, only two out of three phases are excited at any instant of time, leaving the third phase floating.



Figure 2: Back EMF Detection by Virtual Neutral Point

For example, when phase A and phase B conduct current, phase C is floating. This conducting interval lasts 60 electrical degrees, which is called one step. A transition from one step to another Sensor less Control of BLDC Motor.Different step is called commutation. So totally, there are 6 steps in one cycle. The first step is AB, then to AC, to BC, to BA, to CA, to CB and then just repeats this pattern.



Figure 3: Back EMF Detection by Proposed Scheme

Usually, the current is commutated in such way that the current is in phase with the phase back EMF to get the optimal control and maximum torque/ampere. The commutation time is determined by the rotor position. Since the shape of back EMF indicates the rotor position, it is possible to determine the commutation timing if the back EMF is known. The phase current is in phase with the phase back EMF. If the zero crossing of the phase back EMF can be measured, we will know when to commutate the current.

As mentioned before, at one time instant, since only two phases are conducting current, the third winding is open. This opens a window to detect the back EMF in the floating winding. The terminal voltage of the floating winding is

measured. This scheme needs the motor neutral point voltage to get the zero crossing of the back EMF, since the back EMF voltage is referred to the motor neutral point. The terminal voltage is compared to the neutral point, and then the zero crossing of the back EMF can be obtained. In most cases, the motor neutral point is not available.

When virtual neutral point is built by resistors. This scheme is quite simple. It has been used for a long time since the invention. Because of the PWM drive, the neutral point is not a standstill point. The potential of this point is jumping up and down. It generates very high common mode voltage and high frequency noise. So we need voltage dividers and low pass filters to reduce the common mode voltage and smooth the high frequency noise. For instance, if the dc bus voltage is 300 V, the potential of the neutral point can vary from zero to 300 V. The allowable common mode voltage for a comparator is typically a few volts, i.e. 5 V. Obviously, the voltage divider will reduce the signal sensitivity at low speed, especially at start-up where it is needed most .On the other hand, the required low pass filter will induce a fixed delay independent of rotor speed. As the rotor speed increases, the percentage contribution of the delay to the overall period increases. This delay will disturb current alignment with the back EMF and will cause severe problems for commutation at high speed. Consequently, this method tends to have a narrow speed range. In the past, there have been several integrated circuits, which enabled the sensor less operation of the BLDC. A few other schemes for sensor less BLDC motor control were also reported in the literature. The back EMF integration approach has the advantage of reduced switching noise sensitivity and automatically adjustment of the inverter switching instants to changes in the rotor speed. The back EMF integration still has accuracy problems at low speeds the rotor position can be determined based on the stator third harmonic voltage component. The main disadvantage is the relatively low value of the third harmonic voltage at low speed. In, the rotor position information is determined based on the conducting state of freewheeling diodes in the unexcited phase. The sensing circuit is relatively complicated and low speed operation is still a problem The proposed back emf detection method describes that, instead of detecting the zero-crossing point (ZCP) of the non-excited motor back electromagnetic force (EMF) or the average motor terminal to neutral voltage, the true zero-crossing points of back EMF are extracted directly from the supply with simple RC circuits and comparators. In contrast to conventional methods, the neutral voltage is not needed and the diode freewheeling currents in the nonconducted phase are eliminated completely; therefore, the commutation signals are more accurate and insensitive to the common-mode noise. As a result, the proposed method makes it possible to achieve good motor performance over a wide speed range and to simplify the starting procedure.

3. Proposed Direct Back EMF Sensing

Brushless dc (BLDC) motors, with their trapezoidal electromotive force (EMF) profile, requires six discrete rotor position informations for the inverter operation. These are typically generated by Hall- effect switch sensors placed within the motor. However, it is a well-known fact that these sensors have a number of drawbacks. They increase the cost of the motor and need special mechanical arrangements to be mounted. Further, Hall sensors are temperature sensitive, and hence limit the operation of the motor. They could reduce system reliability because of the extra components and wiring. So sensor less method is the reliable method used in harsh environments. There are two independent methods for determining the Hall configuration. The selection of which method to use will depend on the information provided.

- 1. Hall Based Commutation Sequence Provided.
- 2. Back EMF Waveforms.

Hall Based Commutation Sequence Provided:

This method is the straight forward and requires the least amount of effort on the part of the user. This information is usually provided in the form of a diagram or table and may have different titles such as "Block Commutation" or "Brushless DC Motor Timing Diagram".



Figure 4: Simulink model of conversion of Hall Signal in to the Gate pulses of the inverter



Figure 5: Simulink model of Decoder and its Table

Vol 3 Issue 1

The mapping between the Hall states and the three-bit word. Below the binary word representation in are tables that represent the states of the MOSFETs of the half-bridges



Figure 6: Simulink model of conversion into Gate Pulses

4. Simulation Results

A three BLDC motor is fed to the to the inverter bridge and it is connected to controlled voltage source The inverter gates signals are produced by decoding hall effect signals. The three phase output of the inverter is applied to the motors stator windings. From the supply voltage divider is connected, with the RC low pass filter and a compare to zero circuit to produce the back emf for three phases. After simulating the circuit on the Matlab/Simulink, Motor rotor speed. Electromotive force, stator current and electromotive torque are shown in fig.7,8 and



Figure 7: Waveform of the Rotor Speed of the BLDC Motor



Figure 9: Electromagnetic Torque of BLDC Motor

Figure 8: Wavefoms of Stator Current and Electromotive Force

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Figure 10: Back EMF without filters and comparators

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Drive under variable speed reference condition, in variable speed condition we get large ripples but here get low ripples in electromagnetic torque because of effective controller.

A low cost BLDC drive system, which adds only a current sensor and proportional-integral (PI) controller compared to the conventional drive system, the proposed system is to minimize the pulsating torque, it contains large ripplequantities. In this control scheme, the excitation currents are pre shaped based on not only rotor angle but also the velocity is such a way that the motor always generates

torque as requested while the power losses are minimized.

As shown in fig13 all these waveform contains spikes, the circuit with a RC low pass filters is designed and as a result an improved waveform of back emf is obtained as shown in fig.11



Figure 11: ImprovedBack EMF with filters and comparators

5. Conclusion and Future Trends

This paper presented a novel sensorless drive method for BLDC motors. This technique makes it possible to detect the rotor position over a wide speed range from near zero to high speeds. Based on the successful experimental results, the proposed sensorless algorithm with wider speed range can be implemented in various industrial and other applications. This method provides an improved version of the back EMF. Rotor Position is determined by Back EMF ZCD. In this paper it is shown that BLDC motor is a good choice in automotive industry due to higher efficiency, higher power density and higher speed ranges compare to other motor types. BLDC motor model with improved back emf and rotor position detection method is presented in this paper. The proposed model is simulated in MATLAB / SIMULINK.

6. References

- 1. C. Delecluse and D. Grenier, "A measurement method of the exact variations of the self and mutual inductances of a buried permanent magnet synchronous motor and its application to the reduction of torque ripples," in Proc. 5th Int. Workshop Adv. Motion Control, Coimbra, 1998, pp. 191–197.
- 2. R. S. Wallace and D. G. Taylor, "Low-torque-ripple switched reluctance motors for direct-drive robotics," IEEE Trans. Robot. Autom., vol. 7, no. 6, pp. 733–742, Dec. 1991.
- 3. W. S. Newman and J. J. Patel, "Experiments in torque control of the AdeptOne robot," in Proc. IEEE Int. Conf. Robot. Autom., Sacramento, CA, Apr. 1991, pp. 1867–1872.
- 4. F. Filicori, C. G. L. Bianco, and A. Tonielli, "Modeling and control strategies for a variable reluctance direct-drive motor," IEEE Trans. Ind. Electron., vol. 40, no. 1, pp. 105–115, Jan. 1993.
- 5. N. Matsui, T. Makino, and H. Satoh, "Auto compensation of torque ripple of direct drive motor by torque observer," IEEE Trans. Ind. Appl., vol. 29, no. 1, pp. 187–194, Jan.–Feb. 1993.
- 6. S. Ogasawara and H. Akagi, "An approach to position sensorless drive for brushless dc motors," IEEE Trans. Ind. Applicat., vol. 27, pp.928–933, Sept./Oct. 1991.
- A. Consoli, S. Musumeci, A. Raciti, and A. Testa, "Sensorless vector and speed control of brushless motor drives," IEEE Trans. Ind. Electron., vol. 41, pp. 91–96, Feb. 1994.
- 8. J. P. Johnson, M. Ehsani, and Y. Guzelgunler, "Review of sensorless methods for brushless dc," in Proc. IEEE IAS'99 Conf., vol. 1, 1999, pp.143–150.

- 9. M. Tomita, M. Satoh, H. Yamaguchi, S. Doki, and S. Okuma, "Sensorless estimation of rotor position of cylindrical brushless dc motors using eddy current," in Proc. IEEE International Workshop on Advanced Motion Control, vol. 1, 1996, pp. 24–28.
- 10. T. Kim and M. Ehsani, "Advanced sensorless drive techniques for brushless dc motors," U.S. Patent 60/438,949, 2004.
- 11. P. P. Carney and J. F Watson, "Review of position-sensor less operation of permanent-magnet machines," IEEE Trans. Ind. Electron., vol. 53, no2, pp. 352–362, Apr. 2006.
- 12. C.-H. Chen and M.-Y. Cheng, "New cost effective sensor less commutation method for brushless dc motors without phase shift circuit and neutral voltage," IEEE Trans. Power Electron., vol. 22, no. 2, pp. 644–653, Mar.2007
- C.-G. Kim, J.-H.Lee, H.-W.Kim, and M.-J. You, "Study on maximum torque generation for sensor less controlled brushless DC motor with trapezoidal back EMF," IEE Proc.-Electro. Power Appl., vol. 152, no. 2, pp. 277–291, Mar. 2005
- 14. J.X. She and S. Iwasaki, "Sensor less control of ultrahigh-speed PM brushless motor using PLL and third harmonic back EMF," IEEE Trans. Ind. Electron., vol. 53, no. 2, pp. 421–428, Apr. 2006.
- 15. P. Damodharan, R. Sandeep, and K. Vasudevan, "Simple position sensor less starting method for brushless DC motor," IEEE Electro. Power Appl., vol. 2, no. 1, pp. 49–55, Jan. 2008.